

Forces on a body with a vortex-dominated wake

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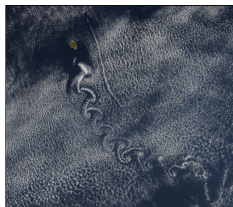
77th annual meeting of the
APS Division of Fluid Dynamics
Salt Lake City, UT

Nov 24, 2024

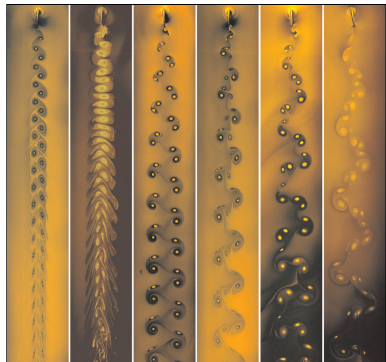
Wakes are often dominated by vortex structures



van Dyke

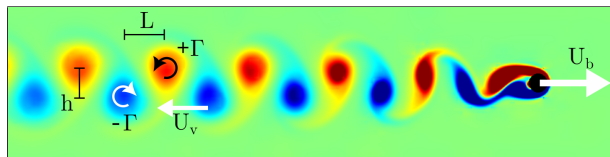


Leeward vortices in the atmosphere



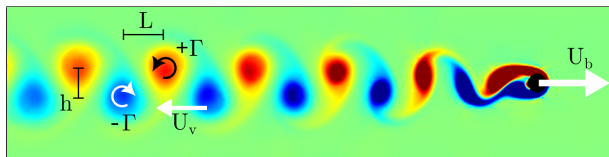
Schnipper et. al (2009)

Kármán found a way to relate the wake vortex structure to forces on the body



numerical simulation of 2D flow past a circular cylinder at low Re

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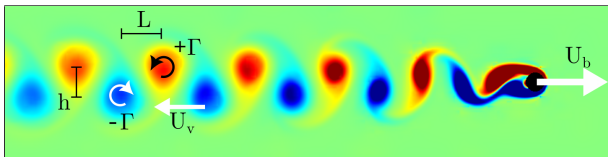


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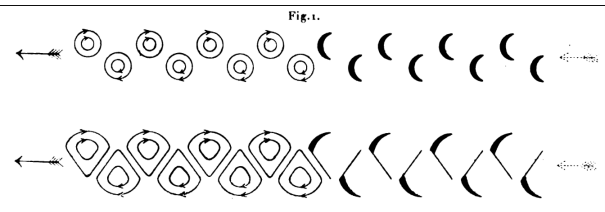
$$F_D = \rho\Gamma \frac{h}{L} (U_b - 2U_v) + \frac{\rho\Gamma^2}{2\pi L} \quad (1)$$

Kármán (1911)

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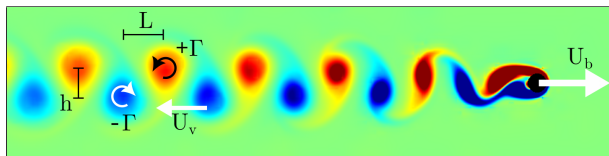
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Kármán (1911)

Henri Bénard, "Formation de centres de giration à l'arrière d'un obstacle en mouvement", Comptes Rendus hebdomadaires des Séances de l'Académie des Sciences 1908

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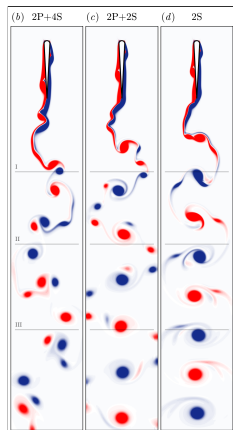
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What assumptions were made by Kármán ?

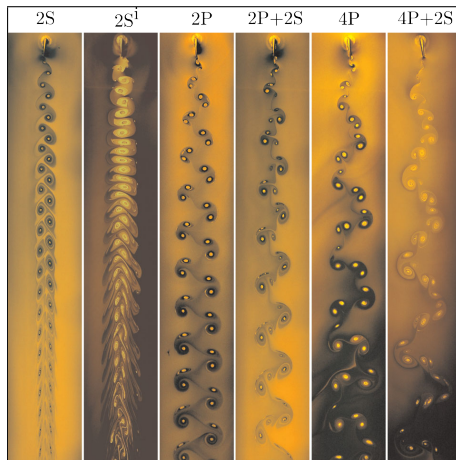
Kármán (1911)

- 2D flow
- Time-periodic flow
- Repeating vortex pattern
- $N = 2$ vortex street
- Horizontal-only motion
- Point vortices, ideal flow
- Vortices in relative equilibrium

Can we generalize Kármán 's drag law for 'exotic' vortex streets?

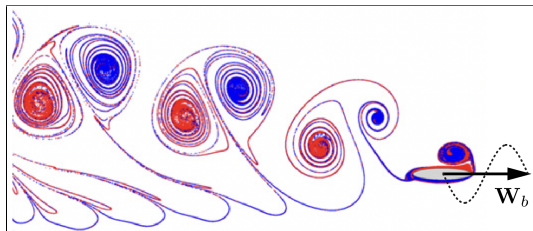


Colvert, Alsalmán & Kanso (2018)



Schnipper et. al (2009)

Forces on a drag-producing bluff body

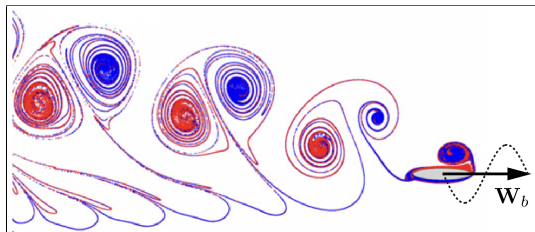


adapted from Kozłowski & Kudela (2014)

We assume:

- 2D flow
- Body moves steadily/periodically with an average velocity $W_b = (U_b, V_b)$
- Equal positive / negative vorticity shed into the wake
- Wake consists of vortices shed along a common axis with possible inclination
- Vortices move collectively with an average velocity $W_v = (U_v, V_v)$
- At this stage, point vortices need not be assumed

Forces on a drag-producing bluff body

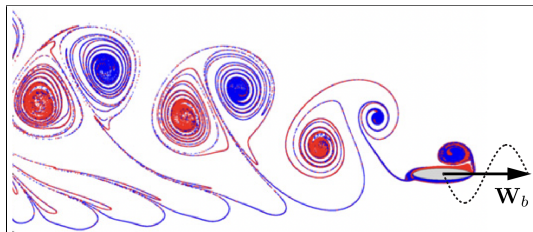


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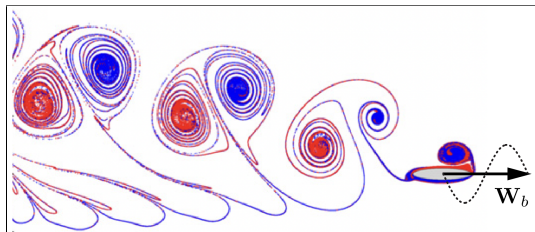


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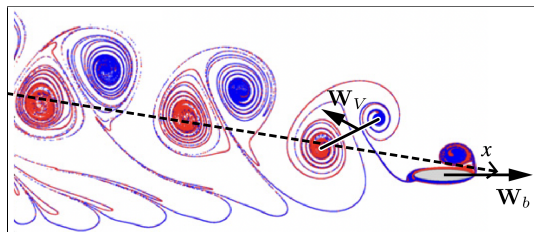


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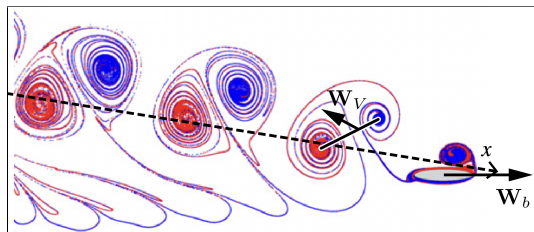


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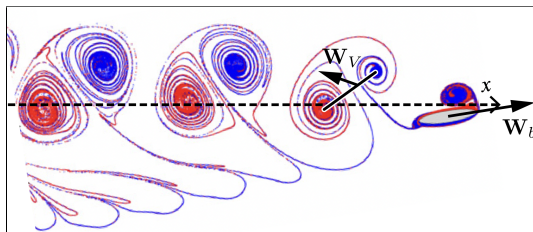


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Consider a control volume moving with the vortices



adapted from Kozłowski & Kudela (2014)

- Control volume moves with \mathbf{W}_v , the **average** speed of the vortices
- Define new variables

$$\mathbf{x}_r = (\xi, \eta) = \mathbf{x} - \mathbf{W}_v t$$

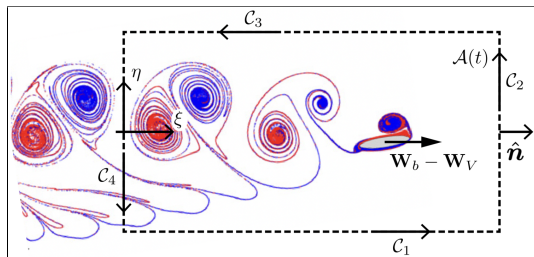
$$\zeta = \xi + i\eta = z - W_v t$$

$$\mathbf{v}_r = (u_r, v_r) = \mathbf{v} - \mathbf{W}_v$$

$$w_r = u_r - iv_r = w - W_v$$

- The body still has motion relative to the control volume
- New vortices are created over time in the interior

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Newton's 2nd Law for the control volume (per unit depth into page)

$$\frac{D}{Dt} \int_{\text{sys}} \rho \mathbf{v} dA = \frac{\partial}{\partial t} \int_{\mathcal{A}(t)} \rho \mathbf{v} dA + \oint_C \rho \mathbf{v} (\mathbf{v} - \mathbf{W}_v) \cdot \mathbf{n} ds = \mathbf{f}(t) \quad (2)$$

Newton's 2nd Law for the control volume (per unit depth into page)

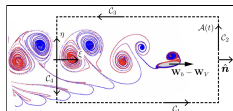
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Rate of change of linear momentum \mathbf{J} inside \mathcal{A} .

$$\mathbf{J}(t; \mathcal{A}) = (J_x, J_y) \equiv \int_{\mathcal{A}(t)} (\mathbf{v}_r + \mathbf{W}_V) dA = \mathbf{J}_r(t; \mathcal{A}) + \mathbf{W}_V A$$

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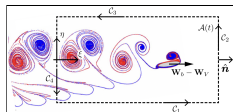
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$$\mathbf{J}_r(t; \mathcal{A}) = \underbrace{\int_{\mathcal{A}(t)} \mathbf{x}_r \times \boldsymbol{\omega}_r dA}_{\text{vortical impulse } \mathbf{I}_{\mathcal{A}}} - \underbrace{\oint_{\mathcal{C}} [\mathbf{x}_r \times (\mathbf{n} \times \mathbf{v}_r)] ds}_{\text{potential impulse } \mathbf{I}_{\mathcal{C}}}$$

\mathbf{J}_r is the sum of a **vortical impulse** and a **potential impulse** — Wu et.al (2015)

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In complex form,

$$\mathbf{I}_{\mathcal{A}}(t; \mathcal{A}) = H_{rx} + iH_{ry} = -i \int_{\mathcal{A}(t)} \zeta \boldsymbol{\omega}_r dA$$

$$\mathbf{I}_C(t; C) = \underbrace{-i \oint_C \phi_r d\zeta}_{\text{Let } \partial_t \text{ of this be } (*)}$$

Flow in \mathcal{A} is allowed to be rotational.

Flow on C is irrotational.

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Flux of linear momentum \mathbf{J} across the contour \mathcal{C}

$$\begin{aligned} \oint_{\mathcal{C}} \rho \mathbf{v} (\mathbf{v} - \mathbf{W}_V) \cdot \mathbf{n} ds &= \rho \oint_{\mathcal{C}} \mathbf{v}_r (\mathbf{v}_r \cdot \mathbf{n}) ds + \rho \mathbf{W}_V \int_{\mathcal{A}(t)} (\nabla_r \cdot \mathbf{v}_r) dA \\ &= \rho \oint \mathbf{v}_r d\psi_r, \quad \text{where } u_r = \frac{\partial \psi_r}{\partial \eta}, \quad v_r = -\frac{\partial \psi_r}{\partial \xi} \end{aligned}$$

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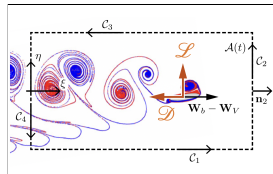
$$\oint_{\mathcal{C}} \rho \mathbf{v} (\mathbf{v} - \mathbf{W}_v) \cdot \mathbf{n} ds = \underbrace{\rho \oint_{\mathcal{C}} \bar{w}_r d\psi_r}_{(**)}$$

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$$\frac{D}{Dt} \int_{\text{sys}} \rho v dA = \frac{\partial}{\partial t} \int_{\mathcal{A}(t)} \rho v dA + \oint_C \rho v (v - W_v) \cdot n ds = \mathbf{f}(t) \quad (2)$$

Instantaneous external force on \mathcal{A} in complex form:

$$\mathbf{f}(t) = f_x(t) + i f_y(t) = \mathcal{D}(t) - i\mathcal{L}(t) + i \oint_C p d\zeta$$

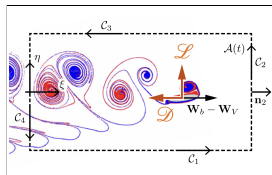


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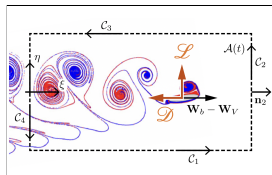
unsteady form of Bernoulli's equation.

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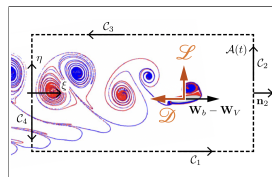
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Terms (*) and (**) appear on both sides of Newton's 2nd Law

Putting it all together

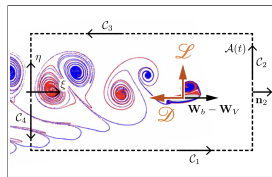
- Take the complex conjugate of Newton's 2nd Law
- Make \mathcal{A} so large that $w_r = W_v$ on C_1 , C_2 , and C_3 (but not on C_4)



Putting it all together

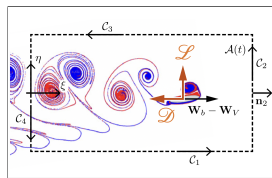
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$$\mathcal{D}(t) + i\mathcal{L}(t) = \underbrace{-i \frac{\rho}{2} \int_{C_4} (w_r + W_v)^2 d\zeta}_{\text{in general time-dependent, call it } \hat{\sigma}(t)} + \rho \frac{\partial}{\partial t} \underbrace{\overline{\mathbf{I}_{\mathcal{A}}(t; \mathcal{A})}}_{\text{vortical impulse inside } \mathcal{A}}$$



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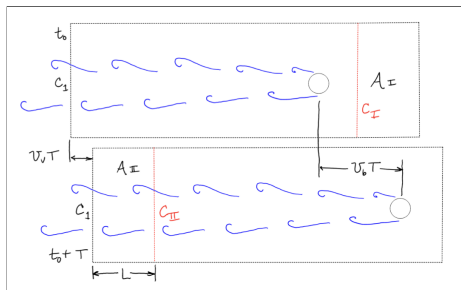
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Integrate over period and divide by T to find the average forces

$$\mathcal{D} + i\mathcal{L} = \frac{1}{T} \int_{t_0}^{t_0+T} \hat{\sigma}(t) dt + \frac{\rho}{T} \underbrace{\Delta \overline{\mathbf{I}_{\mathcal{A}}}}_{\text{change in vortical impulse inside } \mathcal{A} \text{ over one period}}$$

Q. How much does the vortical impulse change over one period?

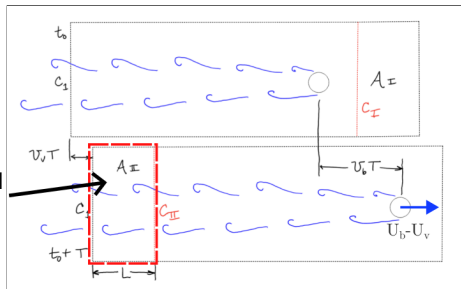
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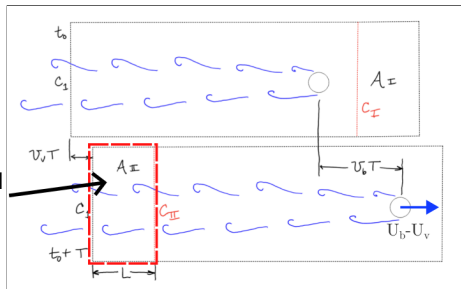
Answer: equal to the vortical impulse in here!



Q. How much does the vortical impulse change over one period?

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Answer: equal to the vortical impulse in here!



Also, the period $T = \frac{L}{U_b - U_v}$, hence we get

$$\mathcal{D} + i\mathcal{L} = \frac{1}{T} \int_{t_0}^{t_0+T} \hat{\sigma}(t) dt + \rho \left(\frac{U_b - U_v}{L} \right) \overline{\mathbf{I}_{A_{II}}}$$

where $\mathbf{I}_{A_{II}} = -i \int_{A_{II}} \zeta \omega_r dA$

Assuming a point-vortex description of the wake ...

For point vortices, $\mathbf{I}_{AII} = P - iQ$

$$\mathcal{D} + i\mathcal{L} = \rho \left(\frac{U_b - U_v}{L} \right) (P + iQ) + \frac{\rho}{4\pi L} \left\{ \sum_{j=1}^N \Gamma_j^2 + \underbrace{\sum_{j=1}^N N \sum_{k=1}^N \Gamma_j \Gamma_k \left[\frac{\pi}{L} (z_j - z_k) \right] \cot \left[\frac{\pi}{L} (z_j - z_k) \right]}_{\text{simplifies to } -4\pi \mathbf{I}_{AII} U_v} \right\}$$

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if the vortices are in relative equilibrium

Also valid for finite-area vortices —
 Saffman & Schatzman (1982) followed by O'Neil (2009)
 have shown this for $N = 2$

We obtain a generalized Kármán-like drag law for N -vortex streets

$$\mathcal{D} + i\mathcal{L} = \rho \left(\frac{U_b - 2U_V}{L} \right) P + \frac{\rho}{4\pi L} \sum_{j=1}^N \Gamma_j^2 + i \left(\dots \right) \quad (3)$$

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Summary & Conclusions

- Given some assumptions about periodic vortex streets with N vortices per period:
- The forces are found to depend on the **vortical impulse** in one period of the wake and the **pressure** on the boundary \mathcal{C}_4
- Forces depend only on the **vortical impulse**, **self-induced speed of the vortices**, and the **sum of the strengths squared**
- Relative equilibria of $N > 2$ vortices on singly-periodic domain are candidates for models of 'exotic' wakes
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Finally, Kármán's ultimate objective with his vortex wake model was to establish a formula for the drag on the bluff body producing the wake. In this he succeeded with what we today know as the *Kármán drag law*. The vortex-street patterns with three vortices per period, e.g., those illustrated in Fig. 8, should also yield a drag law much like von Kármán's. However, it may be possible to extend this further and derive a drag law even for cases where the three-vortex-per-cycle wake is evolving downstream. We leave this as an open problem to which we intend to return.

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Aref, Stremler & Ponta J. Fluid Struct. (2006)

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